

# OP AMPS

## IDEAL AMPLIFIERS + FEEDBACK

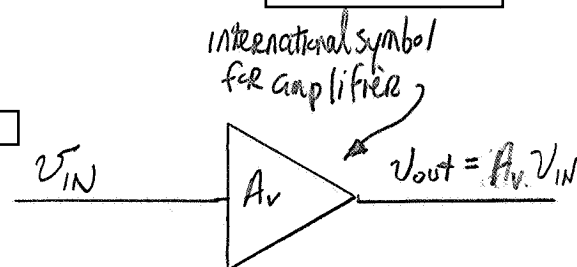
What is an ideal amp?

$$\text{Gain} \equiv \frac{v_{out}}{v_{in}} \rightarrow A_v (\text{gain}) \rightarrow \infty$$

$\xleftarrow{A_v = \text{voltage gain}}$

$$Z_{in} \rightarrow \infty$$

$$Z_{out} \rightarrow 0$$



where  $A_v \equiv \frac{v_{out}}{v_{in}}$  (voltage gain)

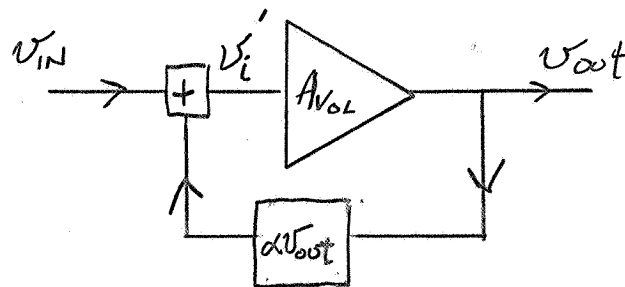
Problem: Gain not constant (cf - transistor  $\beta$ )

Solution: FEEDBACK!!

(block diagram, not schematic  $\rightarrow$ )

$A_{VOL}$  = "open loop" gain

$\alpha$  = fraction of output returned to input  
 $|\alpha| \leq 1$



By def'n of  $A_{VOL}$ ,  $v_{out} \equiv A_{VOL} v_i'$

$$= A_{VOL} (v_{IN} + \alpha v_{out})$$

Gain of entire circuit?

$$A_F \equiv \frac{v_{out}}{v_{IN}} \Big|_{\substack{\text{(algebra)} \\ \text{w/feedback}}} = \frac{A_{VOL}}{1 - \alpha A_{VOL}}$$

$A_F$  = "closed loop gain" (gain w/ Feedback)

CONSEQUENCES?

i) Negative Feedback,  $\alpha < 0$

As  $A_{VOL} \rightarrow \infty$ ,  $A_F \rightarrow \frac{1}{|\alpha|} \rightarrow$  INDEPENDENT OF  $A_{VOL}$ !  
and  $A_F \geq 1$

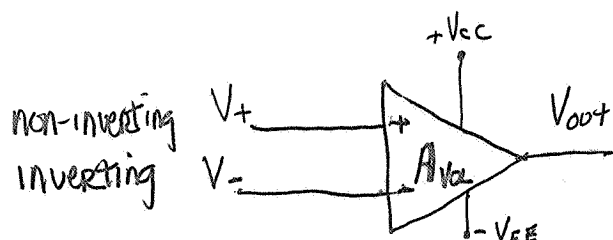
ii) Positive Feedback,  $\alpha > 0$

As  $(\alpha A_{VOL}) \rightarrow 1$ ,  $A_F \rightarrow \infty \rightarrow$  INSTABILITY  
 $\rightarrow$  can result in oscillations

can be good or bad

## Op-AMP - "Operational Amplifier"

- Differential Amp w/ ridiculous gain ( $A \sim 10^5 - 10^6$ )  
to take advantage of negative feedback.
- when used properly, extremely easy to use  
extremely stable



$$\text{GAIN} = A_{VOL} \quad (\text{"voltage gain, open loop"})$$

$$V_{out} = A_{VOL} (V_+ - V_-)$$

NOTE: OP AMPS / ALL IC'S  
must have power supply  
 $+V_{CC}, -V_{EE}$

### Ideal Op Amp Characteristics

a) $Z_{IN} \rightarrow \infty$	Reality $10^6 - 10^{14} \Omega$
b) $Z_{out} \rightarrow 0$	$< 10 \Omega$
c) $A_{VOL} \rightarrow \infty$	$10^5 - 10^6$
d) Bandwidth $\rightarrow \infty$ (frequency range of operation)	1-5 MHz

"GOLDEN RULES" - apply when negative feedback is present

- 1)  $V_+ \approx V_-$  . Output does whatever it takes to make this true  
(via feedback)
- 2)  $I_+ = I_- \approx 0$  inputs draw no current

Armed with these, very powerful but simple circuits can be devised.

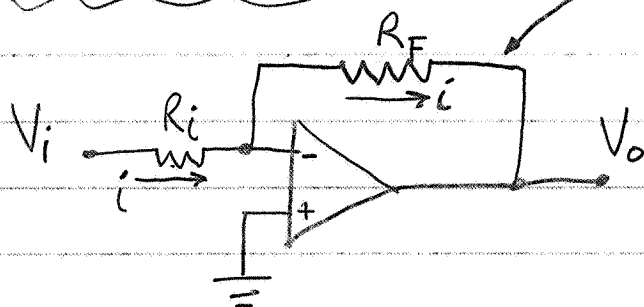
## PRACTICAL LIMITATIONS

- Saturation at rails:  $-V_{EE} < V_{out} < V_{CC}$
- Slew Rate:  $\frac{d}{dt}(V_{out})$  is finite
- Finite input current: must have DC path to inputs/output
- Output Current Limited  $\sim 20-25\text{mA}$
- Frequency Response limited

## BASIC OpAmp Circuits: -

[Combine OpAmp Rules with Kirchhoff, Thevenin]

### A. INVERTING AMP



⇒ works for AC or DC signals

Rule 1: Since  $V_+ \approx V_- \Rightarrow V_- = 0$  "VIRTUAL GROUND"

Rule 2:  $i$  (thru  $R_i$ ) =  $i$  (thru  $R_F$ )

$$i = \frac{V_i - V_-}{R_i} = \frac{V_- - V_o}{R_F}$$

$$A_F = \boxed{\frac{V_o}{V_i} = -\frac{R_F}{R_i}}$$

Independent of  $A_{VOL}$ !!  
(remember emitter follower, independent of  $\beta$ ?)

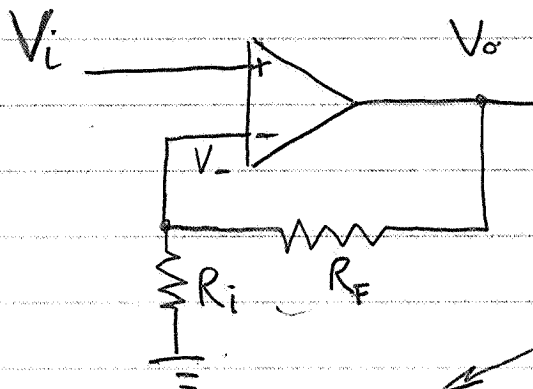
Q - what is limit on gain?

A - saturation at the rails.

Why? There are transistors inside opamps!

## B. Non-Inverting Amp

Note: signal input is to (+) input, but feedback still goes to (-) input. Compare with inverting amp.



Q. why can we use volt divider?

A. NO current flowing out of  $V_-$

2 ways to solve  $\rightarrow V_- = V_o \frac{R_i}{R_i + R_F} \rightarrow$  But  $V_- = V_i$  (golden rule)

Since  $i_{R_F} = i_{R_i}$

$$\frac{V_i - 0}{R_i} = \frac{V_o - V_i}{R_F}$$

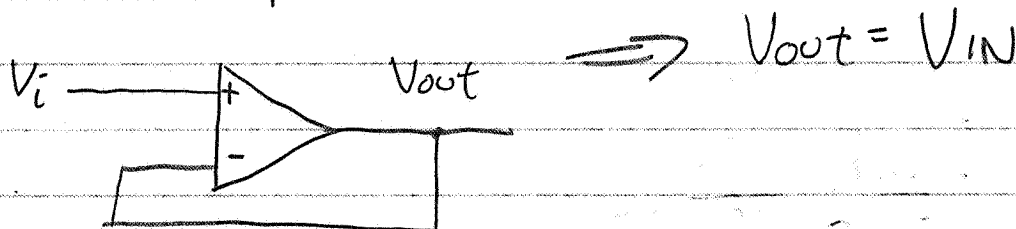
solve  $\Rightarrow$

$$A_F = \frac{V_o}{V_i} = 1 + \frac{R_F}{R_i}$$

## C. Follower or Unity Gain Buffer

Let  $R_F \rightarrow 0$ ,  $R_i \rightarrow \infty$  above.

Then  $A_F = 1$



So What?  $Z_{in} \approx \infty$ ,  $Z_{out} \approx 0$

This is a follower, or impedance "buffer", a chimpanzee can use.

That's what.

# LECTURE 7A

- More opamp circuits
- Non-Ideal OpAmp Models

## MORE CIRCUITS

A. Phototransistors: Current  $\rightarrow$  Voltage converter - (TRANSIMPEDANCE AMP)

transimpedance amp =  
transfer function has units in  
ohms. See result below.

Photodetectors:

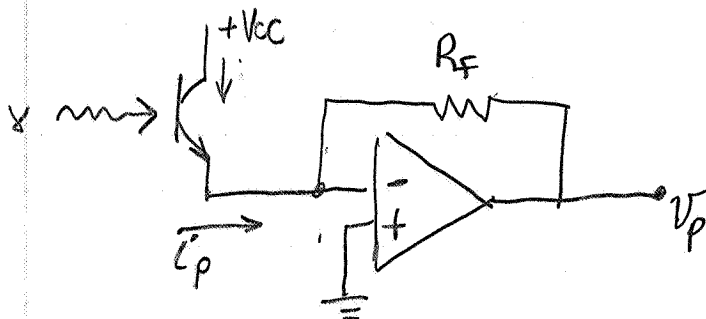
Photodiodes - FAST

Phototransistors = sensitive to very low light

Photomultipliers - " " even less light  
(vacuum tubes, high voltage)

cf neutrino  
detectors

Photodetectors are always current sources - via photoelectric effect.  
In a phototransistor, photons create charge carriers which become  
base current to turn on the transistor. Typical application:



Note: as drawn,  
 $V_{CE} = +V_{CC} - 0$   
 $= +V_{CC}$

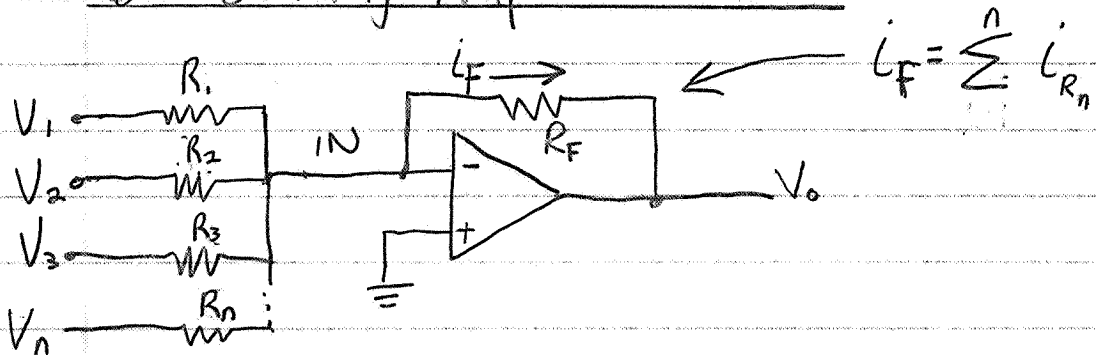
$V_{CE}$  for transistor is fixed at  $(+V_{CC} - 0) = +V_{CC}$ , so that  
 $i_p \sim$  Intensity of incoming light  $\sim$  photons/sec.  
 $\hookrightarrow$  "photocurrent", where

$$i_p = \frac{0 - v_p}{R_F} \Rightarrow v_p = -i_p \cdot R_F$$

output voltage proportional to  $i_p$ .  $R_F$  is the "gain" resistor.

\* || Note the general rule, here and with photodiodes in Lab 2: provide a  
definite external bias  $\Rightarrow$  photocurrent proportional to light intensity

## B. Summing Amp with Gain



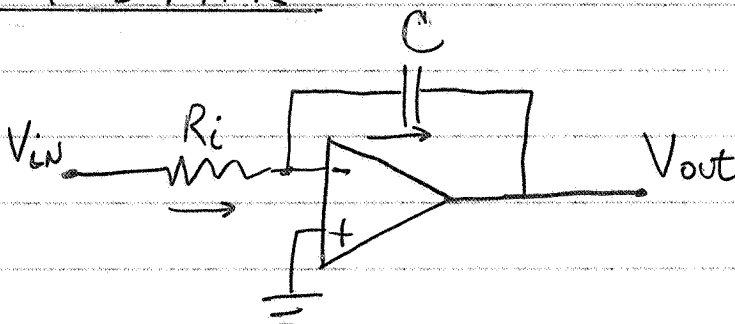
$$V_{out} = -I_F R_F \quad (V_- = 0, \text{ remember?})$$

$$= -R_F \sum I_{R_n} = -R_F \sum \left( \frac{V_n}{R_n} \right)$$

If all  $R_n$  are =,  
 $R_1 = R_2 = R_n = R$ , then

$$V_{out} = -\frac{R_F}{R} \sum V_n$$

## C. INTEGRATOR



$$V_{out} = 0 - V_c$$

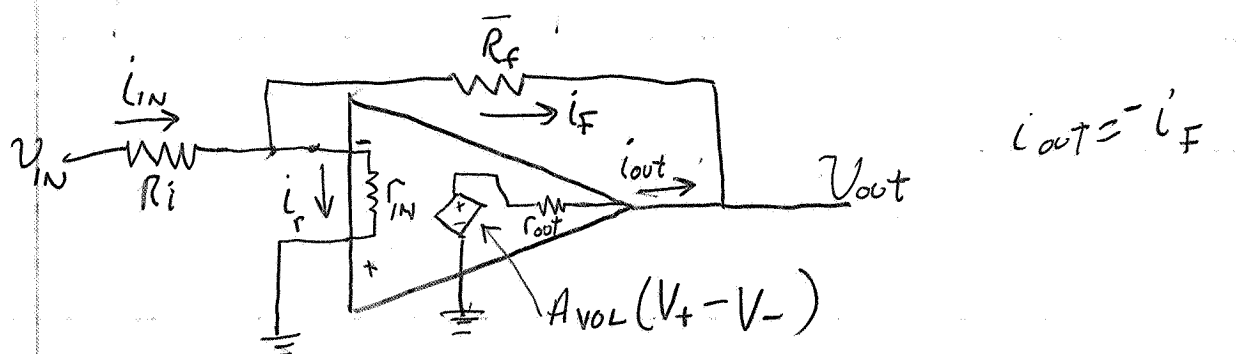
$$\text{But } i_c = C \frac{dV_c}{dt} = -C \frac{dV_{out}}{dt} = \frac{V_{in} - 0}{R}$$

$$\Rightarrow V_{out} = -\frac{1}{RC} \int_0^t V_{in} dt'$$

Compare to plain-vanilla  
 RC circuit: Op amp  
 does not require  
 $V_{out} \ll V_{in} !!$

Pitfall: small asymmetries in input get integrated  $\Rightarrow$  DC offset. See p. 186 in Lab Manual

## NON-IDEAL GAIN



Ignore  $r_{out}$  (since factors of  $i_{out} r_{out}$  are small).  
Relax the  $i_+ = i_- = 0$  assumption.

Then:

$$i_{IN} = i_F + i_r$$

$$(1) \quad \frac{V_{IN} - V_-}{R_i} = \frac{V_- - V_{out}}{R_f} + \frac{V_- - V_+}{r_{IN}}$$

Use the fact that  $V_+ = 0$ , and  $V_{out} = A_{VOL}(V_+ - V_-)$   
 $\Rightarrow V_- = \frac{-V_{out}}{A_{VOL}}$

Substitute for  $V_-$  and  $V_+$  in (1) above, turn the algebra cranks:

$$A_{V_{closed\ loop}} \equiv \frac{V_{out}}{V_{IN}} = \frac{-R_f}{\frac{R_i + R_f}{A_{VOL}} + \frac{R_i R_f}{r_{IN} A_{VOL}} + R_i}$$

As  $A_{VOL} \rightarrow \infty$ ,  $A_V \rightarrow -R_f/R_i$  as before

BUT, what if  $A_{VOL} < \infty$ ?

Let  $R_i = 1k$ ,  $R_f = 10k$ ,  
 $r_{IN} = 10^6 \Omega$ :

Then	$A_{VOL}$ (dB)	$A_V$ (dB)
	$10^5$ (100)	9.999 (20)
	$10^2$ (40)	9.009 (19)
	$10^1$ (20)	4.762 (13.5)
	$10^0$ (0)	0.833 (-1.6)

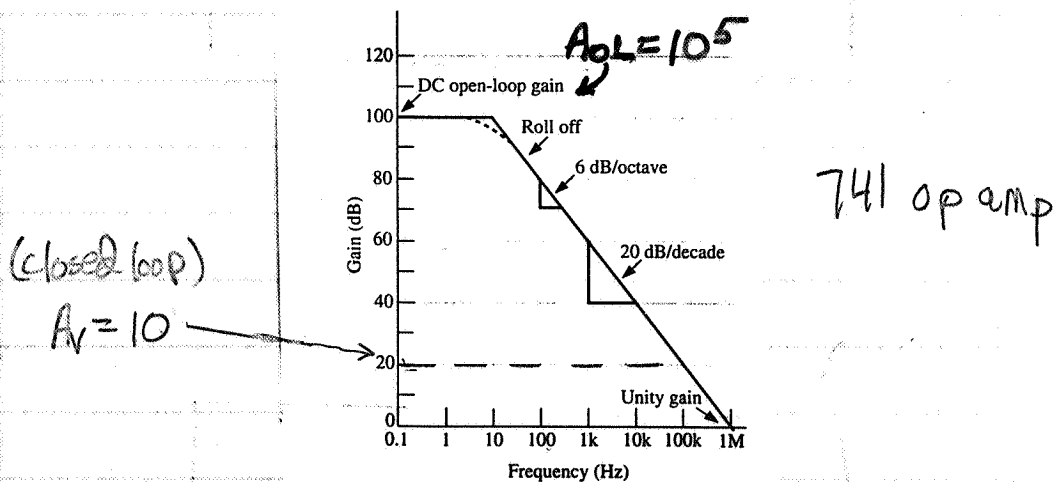
closed loop gain drops  
as  $A_{VOL}$  drops!

Why would  $A_{VOL}$  drop?  $\rightarrow$

What is reality?  $A_{OL} \rightarrow \infty$  and  $\Delta f$  (bandwidth)  $\rightarrow \infty$   
are not true.

$A_{OL}$  is designed to rolloff at high frequencies for stability

Typical gain Rolloff:



SPECS:

- "GAIN BANDWIDTH PRODUCT"

$$A_{OL}(f) \times \Delta f = \text{CONST for a given opamp}$$

"UNITY GAIN BANDWIDTH":  $\Delta f$  when  $A_F = 1$   
 $\sim 4 \text{ MHz (LF411)}$   
 $\sim 1 \text{ MHz (LM741)}$

IMPORTANT CONCLUSIONS:

1) Maintain  $A_F$  (CLOSED LOOP)  $\ll A_{OL}$  (OPEN LOOP)  
at the frequencies of interest

2) Op Amp also behaves like RC low pass