

Precise prediction of NNS HIP components through DEM and FEM modelling

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Content



Introduction

- Purpose of the study
- Process description

Simulation of HIP Process with "Image Analyzed" Densities Distribution

- "Image Analyze" for investigation of initial density distribution
- FEM Simulation

Simulation of HIP Process with DEM simulated Densities Distribution

- Introduction of DEM and Modelling Approach
- Validation, Simulation and Comparison

Summary and Outlook

Purpose of the study

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Welded Capsule (SS304) filled with powder (SS316L) before HIP Process

Capsule (SS304) filled with powder (SS316L) consolidated to full dense after HIP Process

- Anisotropic shrinkage of capsule during PM HIP:
 - Inhomogeneous powder densities distribution in the capsule
 - Temperature gradients and inhomogeneity in the HIP Unit
 - Imperfection of material

Process description



HIP process in general: (a) Capsule production; (b) Filling powder, tapping and vibration; (c) Evacuation; (d) Sealing capsule; (e) Applying high temperature and high pressure; (f) Full density HIPed component

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"Image Analyze" for investigation of initial density distribution



RD [%]

FEM densification model





HIP Simulation with determined densities field in the capsule



RD [%]

55 55

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Process description

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- mathematical description of single objects / particles / granules
- meshless method compared to FEM
- interactions between objects only at contact points

Advantages:

- Few equations which have to be solved for each object
- Forces and motions can be investigated for each single object, which are usually not measureable

Limits in usage:

 Computing time-consuming for real particle systems consists of billions of elements

DEM Modelling Approach







Materials:

- Stainless Steel 316L (Powder)
- SS304 (Underlayment)

Particles: radius 250 µm

Density ρ 7800 kg/m³ Particle radius r 250 µm Young's modulus EPoisson's ratio vCoefficient of restitution $c_{restitution}$ Coefficient of static friction $c_{friction}$ Coefficient of rolling friction $c_{rolling}$

Capacity: 10⁹ Particles

- Iron powder 500 kg
- Ti-Alloys powder 300 kg

Rayleigh time increment:

$$\Delta t_R = \frac{\pi r \sqrt{\rho/G}}{(0.1631 \, v + 0.8766)}$$

Hertz time increment:

$$\Delta t_{H} = 2.87 \left[\frac{(\rho(4/3)\pi r^{3})^{2}}{rE^{2}v_{max}} \right]^{0,2}$$

$$\Delta t = 0,20 \min(\Delta t_R, \Delta t_H)$$

Time increment 0.000001s

Validation - Flow test

Angle of repose





Deviation: 2.9%









Simulation Model

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SS316L Powder Time: Exp. 18.5 s / 50g, Sim. 20.1s / 50g Deviation: 1.6 s , 10.2 %



Filling process using DEM Simulation



Filling process using DEM Simulation

Z = 0





HIP Simulation with determined densities field in the capsule





HIP Simulation with determined densities field in the capsule

Relative Density 1.000 0.971 1200 120 0.942 1000 100 0.913 Temperature [°C] 0.883Pressure [MPa] 80 800 0.854 0.825 600 60 0.796 0.767 400 40 0.738 0.708 200 20 0.679 **Basic HIP Cycle** 0.650 **0**⊣ 0 0 20000 10000 26400 Time [s] Cylinder Capsule Thickness: 1.5 mm Element size~2mm Capsule material: SS304 Powder material: SS316L

Comparison of initial and final shapes



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- Summary
 - Simulation approach with coupled DEM and FEM Modelling has been used to calculate the capsule filling densities and predict the densification behavior of HIP Process.
 - The simulation results correspond well with the experimental measurement.
- Outlook
 - Influences of particle size distribution
 - Influences of pre-desification process, vibration and tapping
 - Influences of more complex shape

Sim. and Exp. of HIP Process chain



RNNTHAA



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